

Vector Optical Modelling for Visible Light Coronagraphy

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http://code935.gsfc.nasa.gov/cube%20Folder/OSCAR/index.html



Contents

- Synopsis of the Study
- · Systems Modeling Approach:
 - Polarization Raytrace
 - Fresnel Diffraction (S & P States)
 - Vector FEM Modeling
 - Component Transfer Functions
 - Systems Level Approach
- · What we will model:
 - Occulters/Pupils/Apodizers
 - Amp/Phase/Polychromatic/Microroughness
 - Misalignments/Deformations
 - Design & Manufacturing Errors
- Expected Results:
 - Tabulate differences in Vector vs Scalar
 - When do we need Vector Theory?
 - Do we have to design w/Vector Theory?
 - Systems level sensitivities
 - Systems level Error Budgeting
 - Validation => Testbeds
- Summary



Studies

Previous Funded Studies:

- TPF Architecture Study (Boeing 07/00 12/01)
 - IR Interferometer and ASA Coronagraph
- Holographic Speckle Correction (GSFC 2002)
 - Photorefractive Polymers w/coronagraph
- ESP NRA (Woodruff, Ridgway, Lyon et.al, 02/02 10/02)
 - Optical design which supports Lyot, SK, ASA
 - Calculate Sensitivities and Error Budget
 - Compare/Contrast Lyot/SK/ASA
 - Woodruff Report (November 2002)

Current Study:

- Development Technologies for the TPF Mission (JPL JYC-572383)
- 2 years w/ optional 3rd year, Oct 2002 Oct 2004
- Lyon, Woodruff, Shiri, Antosik
- 3 Components to Study:
 - 1. Vector vs Scalar Diffraction
 - 2. Static Wavefront Correctors (Fiber Bundle / Phase Plates)
 - 3. Phase & Amplitude Rectification (PAR) Technique
- Couple via Component Transfer Functions (Vector FEM)
- -Systems Level Approach => Sensitivities & Error Budgets
- Tabulate Differences between Scalar & Vector Diffn.



Extra-Solar Planetary NRA Review of Study Results

- ESP NRA (Woodruff, Ridgway, Lyon et.al 02/02 10/02)
 - Phase I:
 - Code V Optical Design (Telescope, AO Bench, Coronagraph)
 - OSCAR Model (Code V & OSCAR Raytrace to < 1e-6)
 - Compare Contrasts of: ASA / Spergel-Kasdin / Lyot Coronagraph
 - Calculate Sensitivities and Error Budget
 - Major Results (Phase I):
 - Contrast Reduction due Mid-freq WFE nearly independent of method!
 - Earths: WFE (3-30 cycles/ap) < λ/10,000 rms, Amp Error < 0.03 %
 - Amp / Wavefront Errors well modelled by:

$$PSF(\lambda/B) = \left[1 - \sigma_A^2\right] \left[1 - k^2 \sigma_{WF}^2\right] PSF_0(\lambda/B) + \sigma_A^2 PSD_A(\lambda/B) + k^2 \sigma_{WF}^2 PSD_{WF}(\lambda/B)$$

$$\left[1-\sigma_{A}^{2}\right]\left[1-k^{2}\sigma_{WF}^{2}\right]$$
: Augmented Strehl Ratio with $PSD_{A}(0)=PSD_{WF}(0)=1$

 $\sigma_{\!\scriptscriptstyle A},\ \sigma_{\!\scriptscriptstyle WF}\ :$ Fraction Amp Error and RMS Wavefront Error

However... All results to date based upon scalar theory



Apodized Square Aperture (ASA)

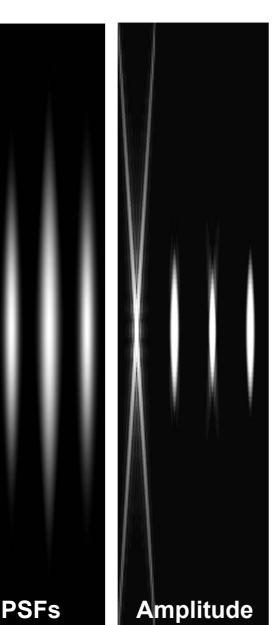
ESPI - Extra-Solar Planet Imager Proposed Concept

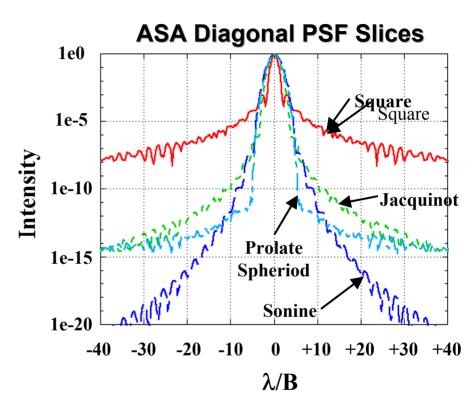


Sonine

Jacquinot

Prolate Spheroid

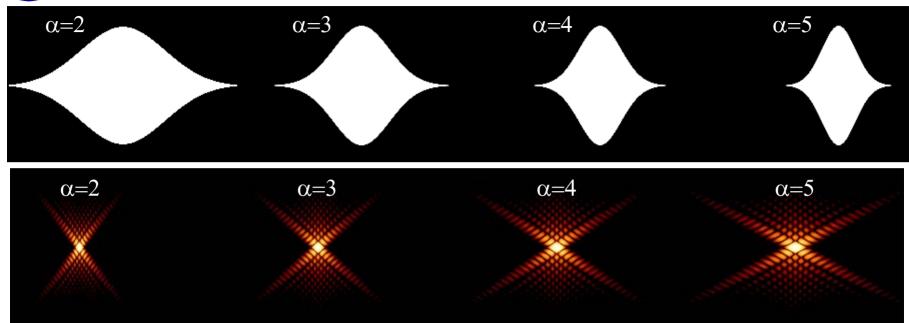




PSFs: λ =0.6 μ m, $\Delta\lambda$ =0.2 μ m. PSFs on same log scale and the Amplitude functions on same linear scale.

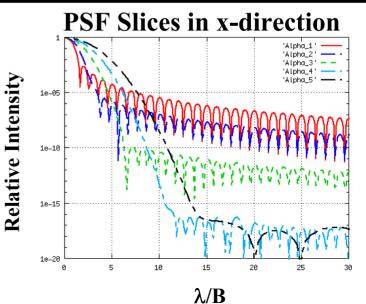


Spergel/Kasdin Pupils Apertures and PSFs



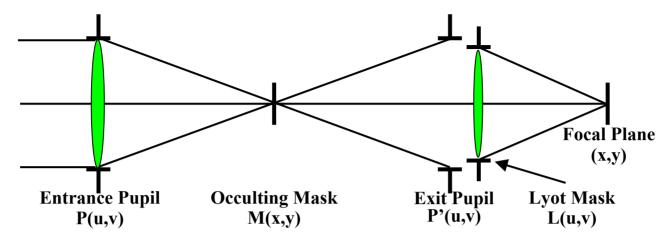
As α is increases:

- Pupils narrow in x
- Null zones decrease in area
- Null depth is deeper
- PSF core broadens

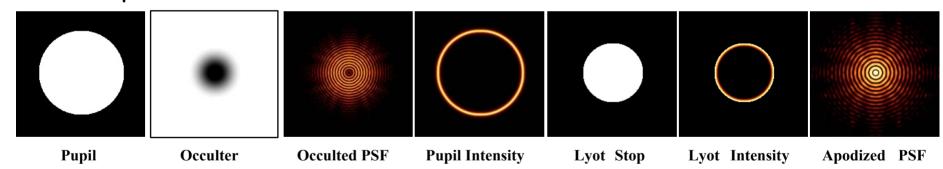




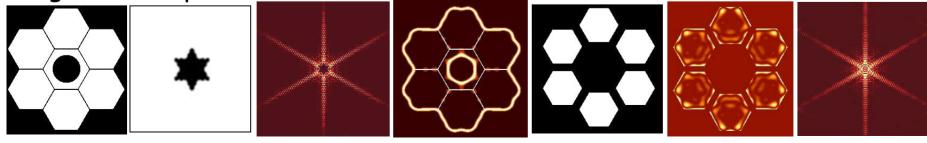
Soft-Edge Lyot Coronagraph



Filled Aperture

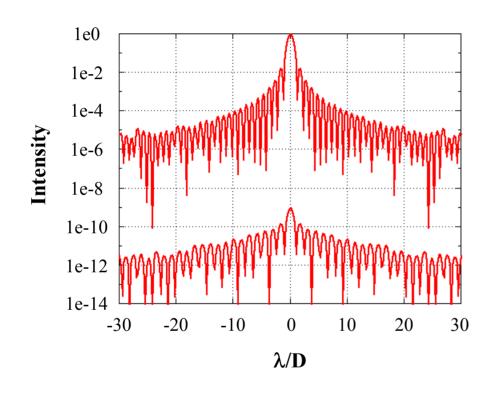


Segmented Aperture





Soft-Edge Occulting Mask PSF Scalar Diffraction Theory



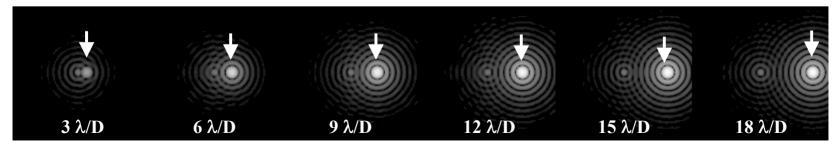
Occulting Mask

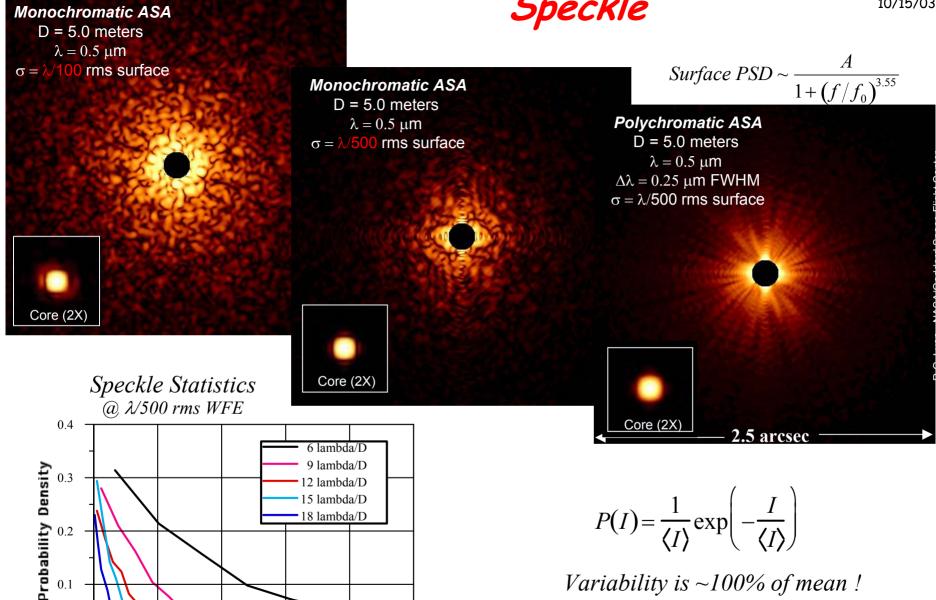
$$T(r) = 1.0 - e^{-\frac{1}{2} \left(\frac{r}{\sigma}\right)^2}$$

$$\sigma = 4 \, \lambda/D$$

Planet/Star at 1e-6 Luminosity Ratio at 75% Lyot Stop

- Soft-edge ring occulting mask, sigma = $4.0 \lambda/D$
- 75% Lyot Stop
- 1e-6 Luminosity Ratio
- Monochromatic
- plots are log-stretched, arrow points to planet.





$$P(I) = \frac{1}{\langle I \rangle} \exp\left(-\frac{I}{\langle I \rangle}\right)$$

Variability is ~100% of mean!

$$mean = \langle I \rangle$$
$$\sigma_I = \langle I \rangle$$

6.0e-07

4.0e-07

0.0

0.0e+00

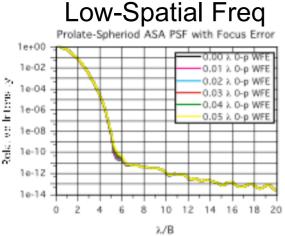
2.0e-07

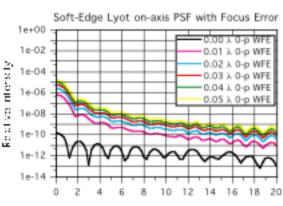
18 lambda/D

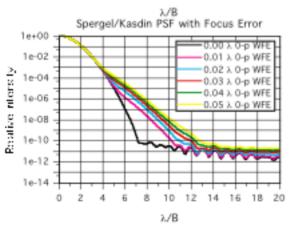
8.0e-07

1.0e-06

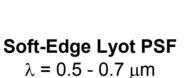
Mid-Spatial Freq

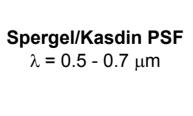


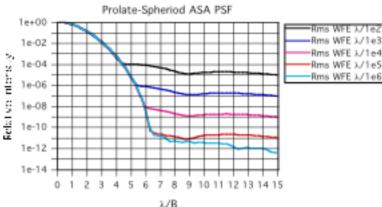


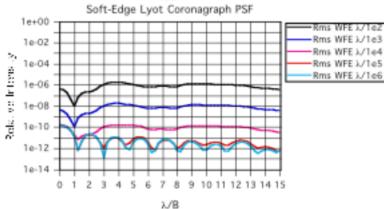


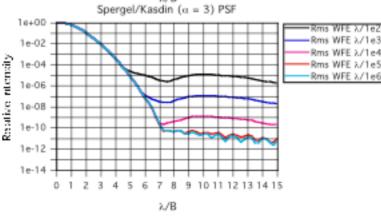
 $\textbf{ASA PSF} \\ \lambda = 0.5 - 0.7 \ \mu \text{m}$











B = Longest Baseline

ALSO:

External Occulters

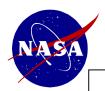
Labeyrie Corrector

HyperTelescopes



Extra-Solar Planetary NRA Review of Study Results

- ESP NRA (Woodruff, Ridgway, Lyon et.al 02/02 10/02)
 - Initially Studied:
 - Apodized Square Apertures
 - Soft-Edge Lyot Coronagraph
 - Spergel/Kasdin Shaped Pupil
 - Effects of:
 - Polychromatic, Wavefront and Amplitude Errors
 - Jitter, Leakage Errors, Random Shape Errors
 - Misalignments, Low-Freq Errors
 - Tabulated Results in Terms of:
 - Contrast, SNR, Detection Zone
 - Sensitivity Analysis and Error Budgeting
 - Documented Results in:
 - -Woodruff, R., Ridgway, S., Lyon, et.al
 Feasibility of and Technology Roadmap for Coronagraphic Approaches
 to TPF Phase I Final Report, NASA NRA-01-055-04
 Extra-Solar Planets Advanced Mission Concepts Type 3 Study, Nov, 2002
 - However... did not contain:
 - Multi-Plane Diffraction (Fresnel)
 - Polarization
 - Full Vector Field Effects on Masks and Occulters
- Development Technologies for TPF (JPL RFP No. JYC-572383)



Scalar vs Vector Theory

Coronagraphs work by Scalar Diffraction Theory

- Scalar Theory is an approximation:
 - (1) Maxwell's Equations => Vector fields in $\vec{E}(\vec{r},t)$ and $\vec{H}(\vec{r},t)$ Scalar theory ignores polarization effects

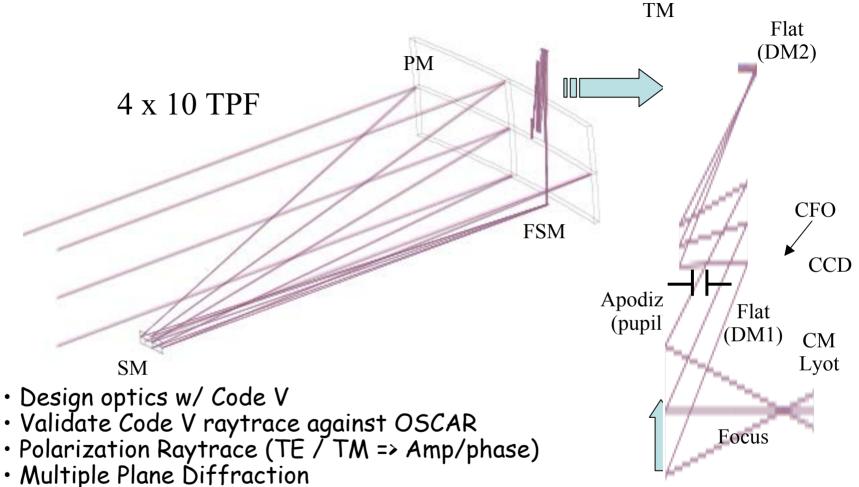
 - Optics introduce polarization shifts, Amp and WF changes
 - (2) Kirchoff Approximation
 - Masks/occulters => infinitely thin perfect conductors
 - Masks/occulters are 3D finite objects w/ n = n + ik
 - (3) Fresnel Approximation
 - 2nd order in phase & paraxial
 - Spherical waves treated as parabolic waves
 - (4) Aberrated Pupil Analysis
 - compresses all phase/amp effects to single diffraction plane.
 - Multiple plane diffraction needed?
- Will Coronagraphs designed w/ Scalar Theory achieve 10-10?

What are implications of Scalar Theory for TPF?

FSM



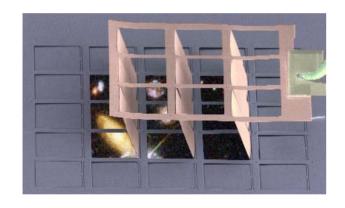
Adopted Full Systems Approach

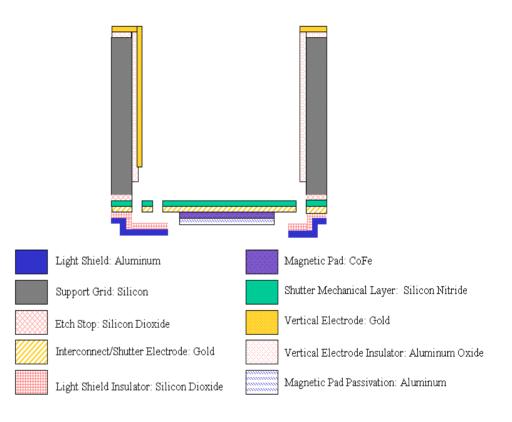


- Multiple Flane Diffraction
 Masks/Occulters via Component Transfer Functions
- Focal Plane Intensities: Lyot, ASA, SK
- · Contrast as function of: misalign/deform/etc...
- · Compare w/ scalar diffraction aberrated pupil analysis



Component Transfer Functions Past Example: JWST/NIRSpec Modeling of MEMS Shutter





NASA

Component Transfer Functions Modeling of MEMS Shutter

Maxwell's Equations are Linear
 Decompose input field into
 Angular plane wave spectrum:

$$C(\alpha) = \int E_{Inc}(x) e^{-i2\pi\alpha(x/\lambda)} dx$$

 Solve Vector FEM for each Angular Plane Wave:

$$E_{Trans}(\alpha, x) = T(\alpha, x)C(\alpha)e^{i2\pi\alpha(x/\lambda)}$$
$$T(\alpha, x) = CTF$$

· Sum over Components

$$E_{Trans}(x) = \int E_{Trans}(\alpha, x) d\alpha$$

- CTF (2D/3D) Requires
 Large scale computing
- <u>But</u> once calculated full vector model can be run on Laptop!
- · Allows 6 DOF & aberr beams
- But not deform/manuf errors requires full model



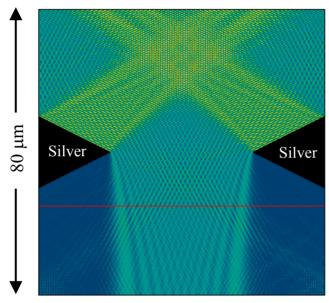
QuickTime[™] and a GIF decompressor are needed to see this picture.



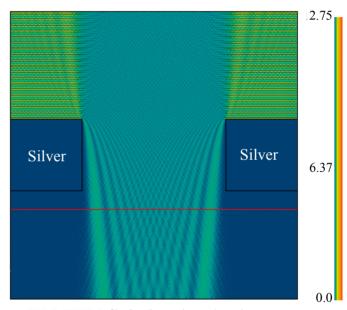
100 mm



Aperture Edge Effects (Ron Shiri's VOM)

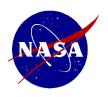


EM FEM Solution, $\lambda = 1$ micron 20 µm thick Silver Bevelled Edge Aperture

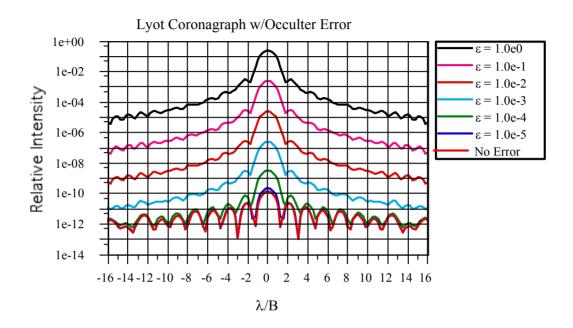


EM FEM Solution, $\lambda = 1$ micron 20 µm thick Silver Square Edge Aperture

- Have to be careful in how edges are made
- · Can model diffraction, skin effects, evanescent modes
- Bevelled edges can give wide angle scatter



Occulter Leakage & Diffraction Effects"



Soft-Edge Lyot on-axis PSFs w/Opacity Error

Polychromatic 0.5 - 0.7 microns 70% Lyot stop

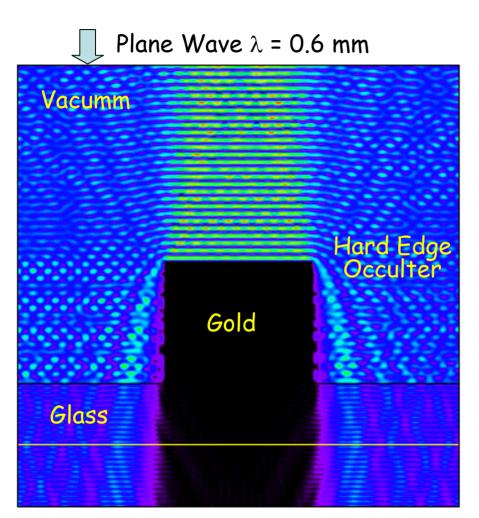
The transmission of the occulter is given by:

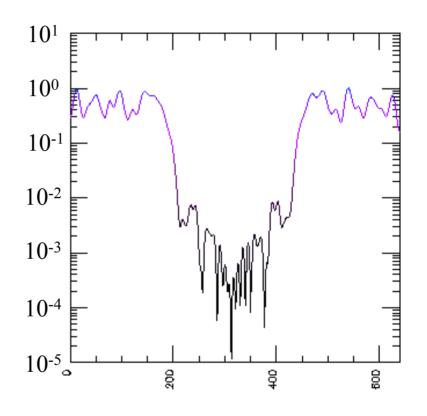
$$T(r) = 1 - (1 - \varepsilon)e^{-\frac{1}{2}\left(\frac{r}{\sigma}\right)^2}$$

Thus ε is **amplitude opacity**, intensity opacity is $\sim \varepsilon^2$



Occulter Leakage & Diffraction (Ron Shiri's VOM)



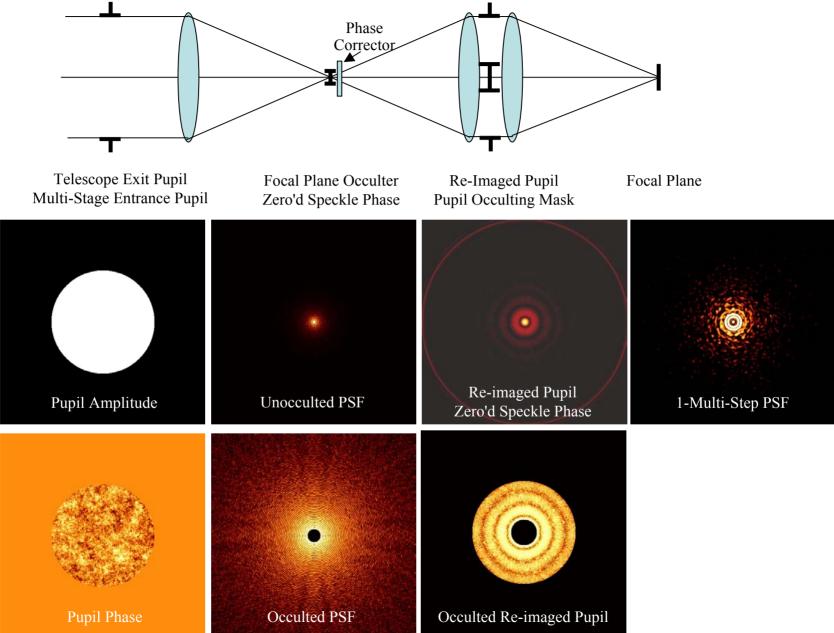


18 μm

 $\lambda = 0.6 \mu m$, 6 μm of Gold thick on 5 μm of glass, 18 x 18 um box

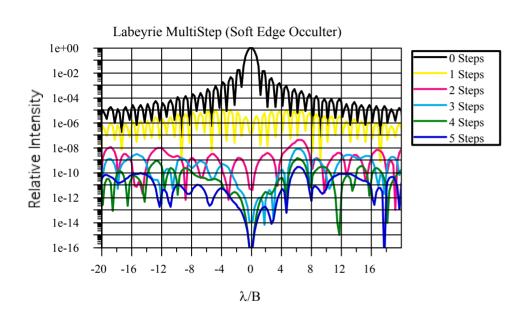


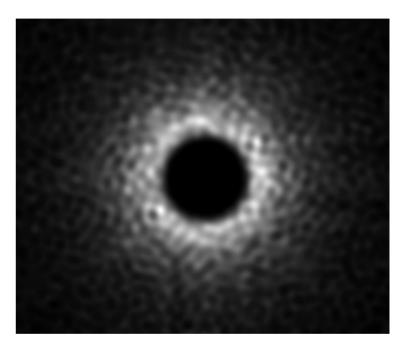
Labeyrie Corrector





Labeyrie Corrector

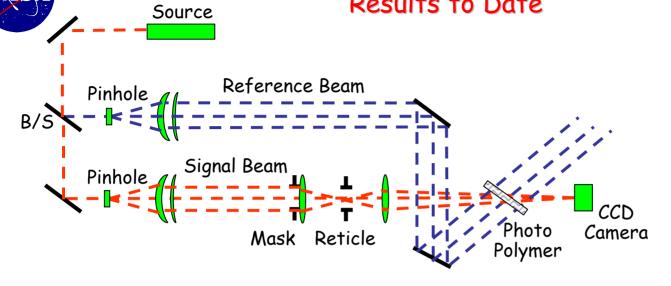


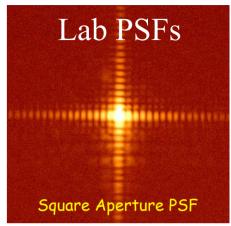


Requires:

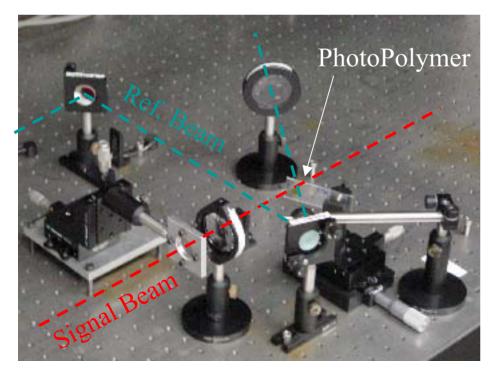
- Wavefront sensing of speckle phases
- Correction of speckle phases need dense DM (or 2 DM method)
- •Need to correct speckle phases to $\lambda/8$
- · Lowers WFE 1 order magn per step
- Lowers PSF wings ~2 orders of magnitude
- Increases Contrast ~2 orders of magnitude

Holographic Speckle Correction Results to Date





PSF with Field Occulter



To Date:

- Built Lab setup (\$70K)
 Manuf & procured photopolymer
 Demo'd Lo-Freq WF Correction
 Next Step: speckle correction
 Out of funds?
- Can be achromatized!



Summary

Current Models:

- OSCAR Optical Systems Characterization and Analysis Research
- Raytrace, Polarization, Pseudo-Nonsequential
- Multiple Diffraction Models: Ang Spect, Fresnel (FFT/Quadrature)
- Filled, Segmented, Interferometric Aperture
- Misalignments, deformations, random surfaces etc...
- Parallel Code (Beowulf Clusters C/MPI)
- Used on previous TPF studies, JWST, Stellar Imager, EASI, etc...
- TPF: ASA/SK/Lyot and External Occulters, HyperTelescopes
- Prep for release through GSFC Tech Commercialization Office.

Expansion of Models:

- Development Technologies for the TPF Mission (JPL JYC-572383)
- 2 years w/optional 3rd year, Oct 2002 Oct 2004
- Lyon, Woodruff, Shiri, Antosik
- Expand Models for:

Vector Diffraction w/Polarization Vector Finite Element Modeling (R. Shiri) Couple FEM to OSCAR via Component Transfer Functions

- Systems Level Approach => Sensitivities & Error Budgets



Backup Slides



OSCAR

Optical Systems Characterization and Analysis Research Software

- Multiple plane diffraction, Fresnel, Fraunhoffer and rigorous Angular Spectrum.
- Segmented apertures and deformable mirrors, influence functions, range limits, clamped, slaved, floating and constrained actuators models.
- Full- and sub-aperture Zernike polynomials.
- power law random surfaces.
- White noise, harmonic and low frequency jitter models.
- Detector effects, MTF, pixelization effects, quantization error, q.e.
- Gaussian and Poisson noise models.
- System radiometry spectral filter functions, optics transmission.
- Coronagraph capability with assortment of masks and Lyot stops.
- Scattering, Surface Scatter, Diamond Turning, Atmosphere
- Scene Modeling Fractal landmass, cloud and water models from LEO/GEO and with scan mirror options.
- Fizeua and Michelson Imaging Interferometer model.
- Polarization raytrace & diffraction
- Inhomogenous wave propagation, (R.Shiri's Ph.D Thesis).
- Shack-Hartmann sensor model etc...

- Disclosed thru TCO
- · Currently undergoing release process
- · 3 Companies have requested use of OSCAR
- · 1 undergoing formal licensing currently



Random Polarization Classical EM Theory

- Treat each polarization seperately in CTF Calculations
- ·Thermal source @ Infinity => Plane waves @ Telescope
- ·Finite source => angular deviation in plane waves
- ·Each time step => single polarization state

$$\vec{E}(\vec{r},t) = \hat{x}E_x(\vec{r},t)\cos\phi(t) + \hat{y}E_y(\vec{r},t)\sin\phi(t)$$

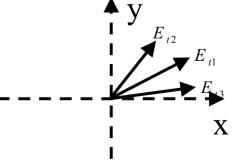
$$\frac{\partial\phi(t)}{\partial t} << \omega \qquad P(\phi(t)) = \frac{1}{2\pi}rect\left(\frac{\phi}{2\pi}\right)$$

·Intensity:

$$I(\vec{r},t) = \left\langle \vec{E}(\vec{r},t) \cdot \vec{E}(\vec{r},t) \right\rangle = E_x(\vec{r},t) E^*_x(\vec{r},t) \left\langle \cos^2 \phi(t) \right\rangle + E_y(\vec{r},t) E^*_y(\vec{r},t) \left\langle \sin^2 \phi(t) \right\rangle$$

$$I(\vec{r},t) = \frac{1}{2} E_x(\vec{r},t) E^*_x(\vec{r},t) + \frac{1}{2} E_y(\vec{r},t) E^*_y(\vec{r},t)$$

Treat polarizations separately
Average output results





Vector Optical Modeling Approach Finite Element Modeling

Each wavelength independent: $\vec{E}(\vec{r},t) = \vec{E}(\vec{r})e^{i2\pi\nu t}$

Inhomog Media => Homog D.E. w/non constant coeffs

$$\nabla^2 \vec{E}(\vec{r}) + \nabla \left(\nabla \ln \varepsilon (\vec{r}) \cdot \vec{E}(\vec{r}) \right) + k^2 \varepsilon (\vec{r}) \vec{E}(\vec{r}) = 0$$

In each homogenous region solve: $\nabla^2 \vec{E}_j(\vec{r}) + k^2 \varepsilon_j \vec{E}_j(\vec{r}) = 0$ w/ boundary conditions:

Solve for TE & TM for each plane wave angle and each λ

$$\vec{E}(\vec{k},z) = E_x(k_x,k_y,z)\hat{x} + E_y(k_x,k_y,z)\hat{y}$$

Decompose arbitrary input field into angular plane wave spectrum

$$E_{x,y}(k_x,k_y,z) = \iint E_{x,y}(x,y,z)e^{-i(k_xx+k_yy)}dxdy$$

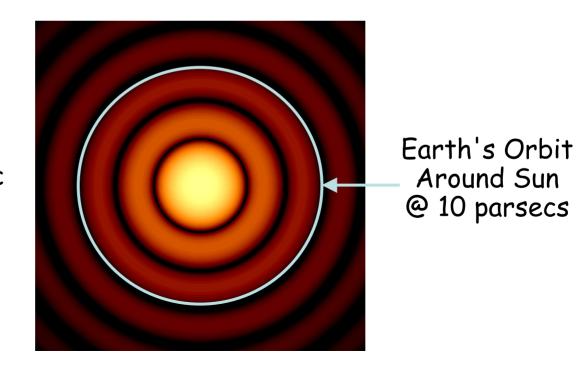
Random Polarization => treat polarization seperately



Statement of the Problem

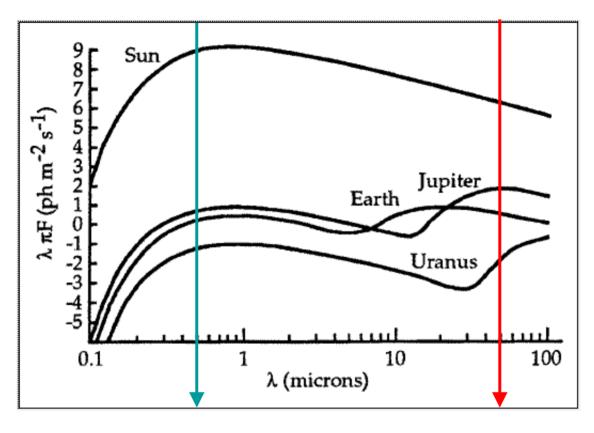


 λ = 0.5 μ m D = 4.0 m 1.22 λ /D = 31 msec Earth ~ 3 - 4 λ /D





Coronagraph vs Interferometer?



Visible Light Coronagraphy

Earth: L_R~10⁻¹⁰

Jupiter: L_R~10-9

IR Interferometry

Earth: $L_R \sim 10^{-7}$

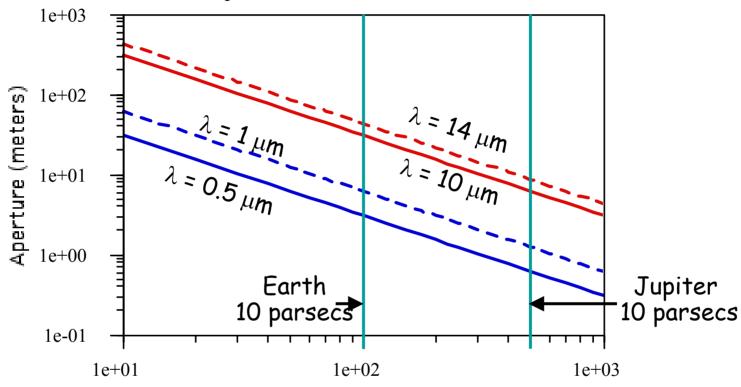
Jupiter: $L_R \sim 10^{-5}$

Interferometry => Significant Advantage in terms of Luminosity Ratio

NASA

However?

Aperture Size vs Resolution



Planet to Stellar Angular Seperation (milli-arcsecs)

Visible Light Coronagraphy

Earth: D ~ 3 - 6 meters

Jupiter: D ~ 0.62 - 1.25 meters

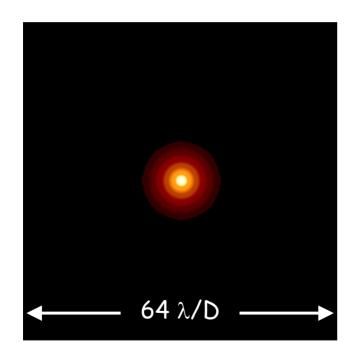
IR Interferometry

Earth: B ~ 30 - 43 meters

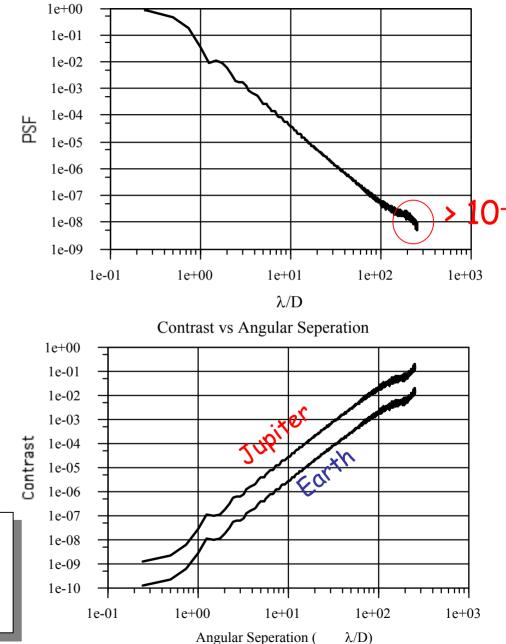
Jupiter: B ~ 6 - 9 meters

Coronagraphy => Significant Advantage in terms of Aperture Size

Why We Need
A Coronagraph?
Why not a conventional
Telescope?



The ratio of the planetary flux to stellar diffracted flux has Contrast < 1 out to ~1000 λ/D !



PSF ($\lambda = 0.5 - 0.8$

um)